

## Basics of Mechanical Engineering-2

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Week 04

Lecture 14

### Tutorial-2 (Casting, Part 2 of 2)

Welcome to the second part of the tutorial on casting that we are discussing this week. We are in the course Basics of Mechanical Engineering II. This is the Manufacturing Processes course. I am Dr. Amandeep Singh. We will discuss casting further in this lecture.

## Sprue and Gate

### Vertical gating Design

For analysis, we use an energy balance equation

$$h_1 + \frac{p_1}{\rho g} + \frac{v_1^2}{2g} + F_1 = h_3 + \frac{p_3}{\rho g} + \frac{v_3^2}{2g} + F_3$$

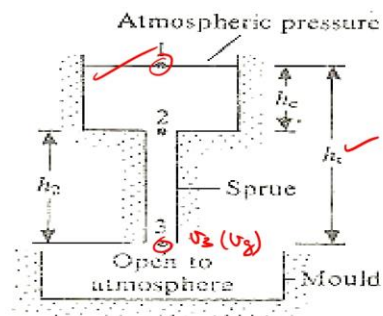
Assuming  $p_1 = p_3$  and level at 1 is maintained constant, so  $v_1 = 0$ ; frictional losses are neglected.

The energy balance between point 1 and 3 gives,

$$gh_t = v_3^2 / 2 \quad \boxed{v_3 = \sqrt{2gh_t}}$$

Here  $v_3$  can be referred as velocity at the sprue base or say gate,  $v_g$

**Continuity equation:** Volumetric flow rate,  $Q = A_1 v_1 = A_3 v_3$



Simple vertical gating



Let us now try to review the sprue and gate design that we discussed in the previous lectures. For analysis, we use the Bernoulli equation, where the pressure head and the velocity head stay constant over time, and the sum of these heads remains unchanged. Now, assuming  $p_1 = p_3$  and the level at 1 is maintained constant, so  $v_1 = 0$ . You can see

this figure. Energy balance between points 1 and 3 gives  $gh_1 = v_3^2 / 2$  which gives  $v_3 = \sqrt{2gh_1}$  where  $v_3$  is the velocity at the sprue base. This is the velocity at the sprue base here, or we can also call this  $v_g$ , which is the velocity at the gate. Or, we can also say this as  $v_g$ , which is the velocity at the gate.

This is the gate entry. 'g' is the gravity coefficient. 'ht' is the height of the sprue. This height ht is given.



## Sprue and Gate

**Problem Statement:** The downsprue leading into the runner of a certain mold has a length = 175 mm. The cross-sectional area at the base of the sprue is 400 mm<sup>2</sup>. The mold cavity has a volume = 0.001 m<sup>3</sup>. Determine

- i. the velocity of the molten metal flowing through the base of the downsprue (mm/s)
- ii. the volume rate of flow (mm<sup>3</sup>/s)
- iii. the time required to fill the mold cavity(s)

$$\begin{aligned}
 i. \quad v_2 &= \sqrt{2gh} \\
 &= \sqrt{2 \times 9.8 \times 1000 \times 175} \\
 &= 1853 \text{ mm/s}
 \end{aligned}$$



60

## Sprue and Gate

**Solution:**

$$\begin{aligned}
 &Q = \text{Volume rate flow} \\
 &Q_1 = Q_2 \\
 &Q = AV \\
 &Q_1 = A_1 v_1 \\
 &Q_2 = A_2 v_2 \\
 &A_1 v_1 = A_2 v_2 \text{ (continuity equation)} \\
 &Q_2 = A_2 v_2 = 400 \times 1853 \text{ mm}^3/\text{s} \\
 &= 741200 \text{ mm}^3/\text{s} \\
 &= 7.412 \times 10^5 \text{ mm}^3/\text{s}
 \end{aligned}$$

$$\begin{aligned}
 iii. \quad Q &= A \cdot \frac{L}{T} \\
 &= \frac{\text{Area} \times \text{length}}{\text{Time}} \\
 \text{Time} &= \frac{\text{Area} \times \text{length}}{Q} \\
 &= \frac{\text{Volume of mould cavity}}{\text{Volume flow rate}} \\
 &= \frac{10^6 \rightarrow 0.001 \text{ m}^3}{7.412 \times 10^5} \\
 &= 1.35 \text{ sec.}
 \end{aligned}$$



Let us start by looking at the problem statement. A down sprue leading into the runner of a certain mold has a length of 175 mm. The cross-sectional area at the base of the sprue is 400 mm<sup>2</sup>. The mold cavity has a volume of 0.001 m<sup>3</sup>. We need to determine the velocity of molten metal flowing through the base of the down sprue in millimeters per second.

$$\begin{aligned} \text{i)} \quad V_2 &= \sqrt{2gh} \\ &= \sqrt{2 \times 9.8 \times 1000 \times 175} = 1853 \text{ mm/s} \end{aligned}$$

$$\text{ii)} \quad Q = \text{Volume rate flow}$$

$$Q_1 = Q_2$$

$$Q = AV$$

$$Q_1 = A_1V_1$$

$$Q_2 = A_2V_2$$

$$A_1V_1 = A_2V_2 \text{ (Continuity Equation)}$$

$$Q_2 = A_2 \times V_2 = 400 \times 1853 = 741200$$

$$= 7.412 \times 10^5 \text{ mm}^3/\text{s}$$

$$\text{iii)} \quad Q = A \cdot v \text{ vector}$$

$$= \text{Area} \times \frac{\text{length}}{\text{Time}}$$

$$\text{Time} = \frac{\text{Area} \times \text{length}}{Q} = \frac{\text{Volume of mould capacity}}{\text{Volume flow rate}} = \frac{10^6}{7.412 \times 10^5} = 1.35 \text{ sec}$$

## Sprue and Gate

**Problem Statement:** The flow rate of liquid metal into the downsprue of a mold = 1 liter/sec. The cross-sectional area at the top of the sprue =  $800 \text{ mm}^2$  and its length = 175 mm. What area should be used at the base of the sprue to avoid aspiration of the molten metal, ( $\text{mm}^2$ )?

**Solution:**

$$1 \text{ liter/sec}; Q = 10^{-3} \text{ m}^3/\text{sec} = 10^6 \text{ mm}^3/\text{sec}$$

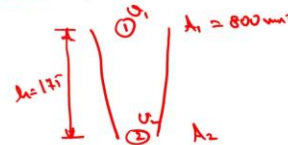
(1000 liter =  $1 \text{ m}^3$   
1 liter =  $10^{-3} \text{ m}^3$ )

$$A_1 v_1 = A_2 v_2 = Q$$

$$A_1 v_1 = 10^6 \text{ mm}^3/\text{s}$$

$$800 \times v_1 = 10^6 \text{ mm}^3/\text{s}$$

$$v_1 = 10^6 / 800 = 1250 \text{ mm/s}$$



## Sprue and Gate

Using Bernoulli's equation:

$$\frac{P_1}{\rho g} + \frac{v_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{v_2^2}{2g} + z_2 \rightarrow \text{At base } z_2 = 0$$

$$\frac{v_1^2}{2g} + z_1 = \frac{v_2^2}{2g}$$

$$\frac{(1250)^2}{2 \times 9.8 \times 1000} + 175 = \frac{v_2^2}{2 \times 9.8 \times 1000}$$

$$v_2 = 2235.173 \text{ mm/sec}$$

Velocity at the base of the sprue to avoid aspiration effect

$$A_2 = \frac{Q}{v_2} = \frac{10^6}{2235.173}$$

$$A_2 = 447.4 \text{ mm}^2$$

Let me look at another problem where the units are in liters per second. Here, we will apply Bernoulli's equation completely, considering the potential head, pressure head, and velocity head. So, in this problem statement that is given: It says the flow rate of liquid metal into the down sprue of a mold is 1 liter per second. The cross-sectional area at the top of the sprue is 800 millimeter square, and its length is 175 millimeter. What area should be used at the base of the sprue to avoid aspiration of the molten metal?

$$1 \text{ liter/sec}; Q = 10^{-3} \text{ m}^3/\text{sec} = 10^6 \text{ mm}^3/\text{sec}$$

$$(1000 \text{ liter} = 1 \text{ m}^3 \text{ so } 1 \text{ liter} = 10^{-3} \text{ m}^3)$$

$$A_1V_1 = A_2V_2 = Q$$

$$A_1V_1 = 10^6 \text{ mm}^3/\text{s}$$

$$800 \times V_1 = 10^6 \text{ mm}^3/\text{s}$$

$$V_1 = 10^6/800 = 1250 \text{ mm/s}$$

$$P_1/\rho g$$

## Sprue and Gate <sup>Q</sup>

**Problem Statement:** Molten metal can be poured into the pouring cup of a sand mold at a steady rate of  $1000 \text{ cm}^3/\text{s}$ . The molten metal overflows the pouring cup and flows into the downsprue. The cross section of the sprue is round, with a diameter at the top =  $3.4 \text{ cm}$ . If the sprue is  $25 \text{ cm}$  long, determine the proper diameter at its base so as to maintain the same volume flow rate (cm).

$$Q = A_1V_1 = A_2V_2$$

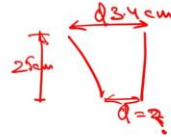
$$V_1 = ? \quad \text{--- (1)}$$

$$\frac{V_1^2}{2g} + 25 = \frac{V_2^2}{2g}$$

$$V_2 = ? \quad \text{--- (2)}$$

$$Q = A_1V_2$$

$$A_2 = ? \quad \text{--- (3)}$$



$$A_2 = 4.043 \text{ cm}^2$$

$$\frac{\pi d_2^2}{4} = A_2 \quad | \quad d_2 = 2.2688 \text{ cm}$$



Let me look at another problem statement that will give us more insights into the design of the sprue and the gate. In this problem, it is given that molten metal is poured into the pouring cup of a sand mold at a steady rate of  $1000 \text{ cm}^3$  per second. We have the value of  $Q$ . This is it. The molten metal overflows the pouring cup and flows into the down sprue.

The cross-section of the sprue is round, with the diameter at the top as 3.4 centimeters. The diameter at the top is given. If I design a sprue here, this diameter is 3.4 centimeters. If the sprue is 25 centimeters long, the height of the sprue will be 25 centimeters.

Determine the proper diameter at the base to maintain the same volume flow rate. The required diameter, D, is the unknown. This can be calculated using a similar setup. We will use the continuity equation,  $Q = A_1 V_1 = A_2 V_2$ . This part will be used to find the value of  $V_1$ , and then we will use this value to determine the required diameter.

Now, using Bernoulli's equation, we set up the equation as  $V_1$  squared by  $2g$  plus  $Z_1$  is equal to  $V_2$  squared by  $2g$ , similar to what was done in the previous problem. So, you will calculate the value of  $V_2$  from here. By substituting this value of  $V_2$  into  $Q = A_2 V_2$ , you will find the value of  $A_2$ . This is step one, step two, and step three. The final value of  $A_2$  is 4.043 square centimeters. Since the sprue is circular, we use the formula pi by four into  $D$  squared is equal to  $A_2$ , which gives me the required diameter.

$D$ , that is the diameter at the base, I will call it  $D_2$ . This is 2.2688 centimeters. You can calculate this and compare your answer with the complete solution provided in the lecture notes. Let me try to solve another interesting problem, where we will calculate the  $g$ -factor. These problems are now something that you are getting familiar with.



## Bottom gating Design

**Assumption:** This is the minimum time required to fill the mould cavity. Since the analysis ignores friction losses and possible constriction of flow in the gating system; the mould-filling time will be longer than what is given by the above equation.

$$h_1 + \frac{p_1}{\rho g} + \frac{v_1^2}{2g} + F_1 = h_3 + \frac{p_3}{\rho g} + \frac{v_3^2}{2g} + F_3$$

Apply Bernoulli's eqn. between points 1 and 3 and between 3 and 4 is equivalent to modifying  $V_3$  equation in the previous gating.

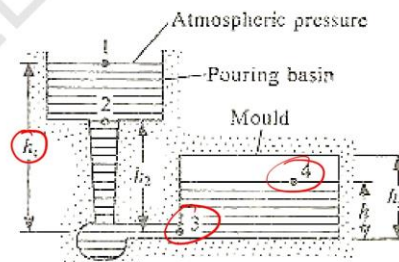
$$v_g = v_3 = \sqrt{2g(h_t - h)}$$

Effective head

Between 3 and 4:

Assume:

- $V_4$  is very small
- All KE at 3 is lost after the liquid metal enters the mould



So, there are certain other problems like this. Before that, let me try to recall one more thing that we discussed in the last lecture.

So,  $v_g = v_3 = \sqrt{2g(h_t - h)}$  If the sprue is designed this way, where  $h_t$  is the total height and  $h$  is the height between points 3 and 4,  $V_4$  is very small between these two points. All



kinetic energy at 3 is lost after the liquid metal enters the mold. So, these are certain assumptions which are taken to calculate or to design the sprue further. Now, here we need to calculate the g-factor.



## Casting Numericals

**Problem Statement:** A horizontal true centrifugal casting operation will be used to make copper tubing. The lengths will be 1.5 m with outside diameter = 15.0 cm, and inside diameter = 12.5 cm. If the rotational speed of the pipe = 1000 rev/min, determine the G-factor.

**Solution:**

$$l = 1.5 \text{ m}$$

$$d_o = 15 \text{ cm}$$

$$d_i = 12.5 \text{ cm}$$

$$N = 1000 \text{ rev/min}$$

$$r = \frac{d}{2}$$

$$r_o = 15/2$$

G-factor: Ratio of centrifugal force to weight

$$= \frac{F_c}{W} = \frac{mv^2/r}{mg} = \frac{v^2}{rg} = \frac{(rw)^2}{rg} = \frac{rw^2}{g}$$

$$= \frac{r \left( \frac{2\pi N}{60} \right)^2}{g} = \frac{15/2 \left( \frac{2\pi \cdot 1000}{60} \right)^2}{9.8 \times 10^2} = 85.83$$



A horizontal true centrifugal casting operation will be used to make copper tubing. The length will be 1.5 meters with an outside diameter of 15 centimeters and an inside diameter of 12.5 centimeters. If the rotational speed of the pipe is 1000 revolutions per minute, determine the g-factor.

$$l = 1.5 \text{ m}$$

$$d_o = 15 \text{ cm}$$

$$d_i = 12.5 \text{ cm}$$

$$N = 1000 \text{ rev/min}$$

$$r_o = 15/2$$

G-factor: Ratio of centrifugal force to weight

$$F_c/W = \frac{mv^2}{mg} = v^2/rg = (rw)^2/rg = rw^2/g$$

$$\frac{r \left( \frac{2\pi N}{60} \right)^2}{g} = \frac{\frac{15}{2} \left( \frac{2\pi 1000}{60} \right)^2}{9.8 \times 10^2} = 85.83$$



## Casting Numericals

**Problem Statement:** True centrifugal casting is performed horizontally to make large diameter copper tube sections. The tubes have a length = 1.0 m, diameter = 0.25 m, and wall thickness = 15 mm.

(a) If the rotational speed of the pipe = 700 rev/min, determine the G-factor on the molten metal.

(b) Is the rotational speed sufficient to avoid "rain"?

(c) What volume of molten metal must be poured into the mold to make the casting if solidification shrinkage and contraction after solidification are considered ( $m^3$ )?

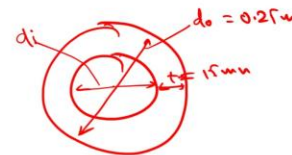
Solidification shrinkage for copper = 4.5%, and solid thermal contraction = 7.5%



## Casting Numericals

**Solution:**

$$\begin{aligned} l &= 1 \text{ m} \\ d_o &= 0.25 \text{ m} \\ t &= 15 \text{ mm} \\ N &= 700 \text{ rev/min} \\ d_i &= d_o - 2t \\ &= 0.25 - 2 \times (15 \times 10^{-3}) \\ &= 0.22 \text{ m} \end{aligned}$$



$$\begin{aligned} \text{a) G-factor} &= \frac{F_c}{W} = \frac{R\omega^2}{g} = \frac{d_o/2 \times \left( \frac{2\pi N}{60} \right)^2}{g} \\ &= \frac{0.25}{2} \times \frac{(2 \times 3.14 \times 700)^2}{60^2} \\ &= 9.8 \end{aligned}$$

$$= 68.46$$

b)  $60 < 68.46 < 120$ ; it lies in the optimum range  
 $\therefore$  "Rain" is avoided





## Casting Numericals

e)  $V =$  Find Volume of product

$$= \frac{\pi}{4} (d_o^2 - d_i^2) \times L$$

$$= \frac{\pi}{4} (0.25^2 - 0.22^2) \times 1 = 0.011074 \text{ m}^3$$

✓ Shrinkage = 4.5%

✓ Contraction = 7.5%

$$V' = \frac{V}{(1 - \text{shrinkage}) (1 - \text{contraction})}$$

$$= \frac{0.011074}{\left(1 - \frac{4.5}{100}\right) \left(1 - \frac{7.5}{100}\right)}$$

$$= 0.012536 \text{ m}^3$$



A similar problem in calculating the G factor: Tube centrifugal casting is performed horizontally to make large-diameter copper tube sections. The tubes have a length of 1.0 millimeter, a diameter of 0.25 millimeter, and a wall thickness of 15 millimeters. That means I have the length as 1 meter, the diameter as 0.25 meters, and the wall thickness as 15 millimeters. I will call the thickness T as 15 millimeters. Now, it says that if the rotational speed of the pipe is 700 revolutions per minute, That means the rotational speed, denoted as n, is given as 700 revolutions per minute.

Then, it says, determine the G-factor on the molten metal. Part B: Is the rotational speed sufficient to avoid rain? What volume of molten metal must be poured into the mold to make the casting if solidification shrinkage and contraction after solidification are considered? The solidification shrinkage for copper is given as 4.5 percent, and its thermal contraction is 7.5 percent.

$$l = 1 \text{ m}$$

$$d_o = 0.25 \text{ m}$$

$$t = 15 \text{ mm}$$

$$N = 700 \text{ rev/min}$$

$$d_i = d_o - 2t = 0.25 - 2 \times (15 \times 10^{-3}) = 0.22 \text{ m}$$

$$a) \text{ G-factor} = Fc/W = rw^2/g = \frac{\frac{d_o}{2} \left(\frac{2\pi N}{60}\right)^2}{9.8} = \frac{0.25 \left(\frac{2 \times 3.14 \times 700}{60}\right)^2}{9.8} = 68.46$$

b)  $60 < 68.46 < 120$ ; it lies in the optimum range. Therefore, Rain is avoided.

c)  $V = \text{Volume of Product}$

$$= \pi/4 (d_o^2 - d_i^2) \times L$$

$$= \pi/4 (0.25^2 - 0.22^2) \times 1 = 0.011074 \text{ m}^3$$

$$\text{Shrinkage} = 4.5 \%$$

$$\text{Contraction} = 7.5 \%$$

$$V' = \frac{V}{(1-\text{Shrinkage})(1-\text{contraction})}$$
$$= \frac{V}{\left(1-\frac{4.5}{100}\right)\left(1-\frac{7.5}{100}\right)} = 0.012536 \text{ m}^3$$

With this, I am closing this tutorial session. We will meet in the next lecture, where I will talk about a certain laboratory demonstration, the virtual laboratory demonstration in casting. Thank you.