

Fluid Dynamics And Turbo Machines.
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Part B.
Module-2.
Tutorial-1.
Tutorial: Week 6.

Good afternoon, so we come to the end of this week 6 and today we will take up some tutorial problems and we will do it step-by-step so that we have the familiarity with the concepts that are discussed. And which will also help you in doing the tutorials in this week. So let us look at the first problem.

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FLUID DYNAMICS AND TURBOMACHINES PART-B Module-02 - Tutorial 2

1) Absolute velocity of water at impeller exit is 14 m/s at an angle of 18° (α_2). The blade peripheral speed at the exit is 25 m/s, and the shaft speed is 1450 rpm. Whirl component of the absolute velocity at the inlet is zero. The flow rate is 18.0 litres/s. Find (a) the magnitude of the relative velocity and its flow angle β_2 and (b) the power required if pump efficiency is 100%.

$C_1 = C_{m1}$

$C_2 = 14 \text{ m/s} \quad \alpha_2 = 18^\circ$

$N = 1450 \text{ rpm}$

$U_2 = 25 \text{ m/s}$

$\dot{V} = 18 \text{ litre/s}$
 $= 0.018 \text{ m}^3/\text{s}$

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The first problem says that an absolute velocity of water at the impeller exit is 14 metres per second at an angle of 18 degrees. So when we talk about absolute velocities, the angle, corresponding angle is Alpha 2. In the problem that we will be giving you in the tutorial set we will not mention it as alpha 2. In the worked out example today I am talking about alpha 2 so that you can connect and remember that alpha is the angle which the absolute velocity makes.

The blade peripheral speed U at the exit is 25 metres per seconds, shaft speed is 1450 rpm, whirl component of the absolute velocity at inlet is zero. The flow rate is 18 metre per seconds, please take care of the units, you have to be consistent, so convert this into metres cube per seconds and find the magnitude of the relative velocity and its flow angle beta 2,

also find out the power required assuming that the pump of efficiency is 100 percent. We will solve this problem for pump efficiency of 100 percent.

If the pump efficiency is different from 100 percent, you should be able to take it into consideration by the suitable factor of the efficiency. So in this sort of problems, my suggestion is always draw the velocity triangle and write down what all are given. So this is the exit velocity triangle with C_2 is absolute velocities, W_2 is the relative velocity and U_2 use the blade peripheral velocity on the pressure side or the exit. Alpha 2 and beta 2 are the corresponding angles, C_{u2} is a whirl component and C_{m2} is the meridional component.

And at the inlet, since it is given that the whirl component of the absolute velocity is zero, so we can write C_1 equals C_{m1} and the corresponding other velocities are U_1 and W_1 . What is given as C_2 equal to 14 metre per seconds and alpha 2 equal to 18 degrees. We also know that the RPM is given 1450 as N , we have written, U_2 as 25 metres per seconds, C_{u1} is zero. Volume flow rate is 18 litres per seconds as I said convert it into metres cube per seconds. We need to find out the relative velocity, means we need to look at the triangle at the pressure side.

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$C_{2u} = C_2 \cos \alpha_2 = 13.3 \text{ m/s}$

$C_{2m} = C_2 \sin \alpha_2 = 4.33 \text{ m/s}$

$W_{2u} = U_2 - C_{2u} = 11.69 \text{ m/s}$

$W_{2m} = C_{2m} = 4.33 \text{ m/s}$

$W_2 = \sqrt{W_{2m}^2 + W_{2u}^2}$
= 12.46 m/s

$\beta_2 = \tan^{-1} \left(\frac{W_{2m}}{W_{2u}} \right)$
= 20.3°

$P_c = P_{bl} = \rho \dot{V} (U_2 C_{2u} - U_1 C_{1u})$

$P_c = 5.99 \text{ kW}$

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So let us look at the triangles again okay. So we are talking about C_{2u} or C_{u2} , the notations can be used in different ways but both are consistent. So C_{u2} or C_{2u} are the same quantity is $C \cos \alpha_2$ which is 13.3 metres per second, you can work it out, the values you can get from the relationship. And C_{m2} is related with the sin alpha, so C_2 multiplied by sin Alpha 2 is 4.33 metres per second, thus we know this is 4.33 metres per second and C_{u2}

is 13.33 13.3 metres per second. So what is $W U_2$, $W U_2$ is the corresponding projection of W_2 along U_2 , so this distance.

This distance is what we are talking about. This distance is $W U_2$. And here when we are talking about it, we can find out the $W U_2$ or $W_2 U$ is U_2 minus $V_2 U$ is 11.69 metres per second and we know that C_{2M} or C_{2M} equal to $W_2 M$ and it is equal to 4.33 metres per seconds. So now to get W_2 is nothing, we know $W_2 M$ and $W_2 U$, so we can find out W_2 to be 12.46 metres per seconds and β_2 can be found out by the tan of β_2 we know is $W_2 M$ by $W_2 U$ and hence β_2 is tan inverse of $W_2 M$ by $W_2 U$ which is 20.3 degrees.

And coupling power, in this case is a blade specific power because there are no losses, we have talked about hundred percent efficiency, so we can see coupling power equal to PBL is equal to $\rho V \dot{U}_2 C_{U_2}$ minus $U_1 C_1$. But C_{U_1} is zero and hence we get the coupling power is 5.99 kilowatt. We can continue with this problem and add some more complexities.

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2) Continuing from previous problem, find the outer diameter (D_2). If inner diameter (D_1) is $0.6D_2$, determine inlet blade angle (β_1) if meridional velocity is constant.

$C_2 = 14 \text{ m/s}$ $\alpha_2 = 18^\circ$
 $N = 1450 \text{ rpm}$
 $U_2 = 25 \text{ m/s}$
 $\dot{V} = 18 \text{ litre/s}$
 $= 0.018 \text{ m}^3/\text{s}$

$U_2 = \frac{\pi N D_2}{60}$

$D_2 = \frac{60 U_2}{\pi N} = 0.329 \text{ m}$

$U_1 = \frac{D_1}{D_2} \Rightarrow U_1 = U_2 \frac{D_1}{D_2} = 15 \text{ m/s}$

$C_{1m} = C_{2m} = 4.33 \text{ m/s}$

$\beta_1 = \tan^{-1} \left(\frac{C_{1m}}{U_1} \right) = 16.1^\circ$

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We can say that the outer diameter of the same pump which we have talked about, we need to find out. And if the inner diameter is 60 percent of the outer diameter, can we find the inlet blade angle β_1 ? It is given that the meridional velocity is constant, which means C_{1M} equal to C_{2M} . So as before we will draw the velocity triangles and taking the data which we have already obtained in the first problem and along with what is given, let us write down. It is already given that C_2 is 14 metres per second and α_2 is 18 degrees.

The blade rotational speed was also given along with the blade peripheral speed, volume flow rate was also given. We know the relationship that U_2 is equal to $\pi N D_2$ by 60 and hence D_2 can be obtained as 0.329 metres. We know that U_1 by U_2 is equal to D_1 by D_2 . Basically U_2 is $\pi N D_2$ by 60 and U_1 is $\pi N D_1$ by 60, hence U_1 by U_2 will be D_1 by D_2 . And we can get U_1 as 15 metres per second. Now look at the velocity triangle at the inlet or the suction side. We know U_1 and since it is given that C_{m1} equal to C_{m2} , we can say that both are 4.33 metres per second and hence we can find out β_1 .

β_1 is $\tan^{-1} C_{m1} / U_1$ which is 16.1 degree. Okay. So what did we do, we have found out the velocity triangle information given in the outlet or the pressure surface and then obtained the corresponding relationships which we required for the inlet or the suction surface, suction side.

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3) Continuing from previous problem, find the blade height at the impeller exit (b₂) neglecting vane thickness.

$C_2 = 14 \text{ m/s}$ $\alpha_2 = 18^\circ$
 $N = 1450 \text{ rpm}$
 $U_2 = 25 \text{ m/s}$
 $\dot{V} = 18 \text{ litre/s}$
 $= 0.018 \text{ m}^3/\text{s}$
 $D_2 = 0.329 \text{ m}$
 $C_{2m} = 4.33 \text{ m/s}$

Assuming zero thickness

$\dot{V} = \pi D_2 b_2 C_{2m}$
 $b_2 = 4 \text{ mm}$

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And we can continue with this same problem, we want to find out the blade height at the impeller exit which is b_2 neglecting the vane thickness. That is we know the volume flow rate and you know from the classes that we have done in the last class, we talked about the volume flow rate in case of a radial flow machine is nothing but πD times B times the corresponding meridional velocity. So we will use that relationship here.

As before we are talking about the velocity triangles, we write down whatever are given, the C_2 , α_2 , U_2 , volume flow rate and diameter, we have also obtained diameter D_2 . So we can write, and we know the C_{2M} , we have calculated and obtained it in the first problem,

now assuming that zero thickness of the vanes we can write that $V \cdot$ is nothing but $\pi D B C_2 M$ which will give me B to be 4 millimetres. Now you can do this problem yourself by assuming that the blades occupy let us say 5 percent of the vane passage.

Or blade thickness is accounting for 5 percent. So then you can write a factor with 5 here which is equal to 0.95 and you can find out B . I leave that as an exercise for you and a similar problem where the blade height has to be obtained in case of a finite vane thickness is given for your practice.

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4) Continuing from previous problem, find the degree of reaction

$C_2 = 14 \text{ m/s}$
 $U_2 = 25 \text{ m/s}$
 $W_2 = 12.46 \text{ m/s}$
 $U_1 = 15 \text{ m/s}$
 $C_1 = 4.33 \text{ m/s}$
 $W_1 = \sqrt{C_1^2 + U_1^2} = 15.61 \text{ m/s}$

$$R = \frac{(U_2^2 - U_1^2) + (W_1^2 - W_2^2)}{(C_2^2 - C_1^2) + (U_2^2 - U_1^2) + (W_1^2 - W_2^2)} = 0.73$$

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Finally I come to the last problem that we want to find out the degree of reaction. We know from the previous 3 problems that C_2 is equal to 14 metres per second, we know U_2 is 25 metres per second, we know W_2 is equal to 12.46 metres per second. All these were either given or obtained in problem 1. Now we also know from the 2nd problem that U_1 is 15 metres per second and C_1 is nothing but C_{M1} as I have written here and C_{M1} equal to C_{M2} , it was also given.

So we can say it is 4.33 metres per second and we can find out now W_1 here in this velocity triangles, right angle velocity triangle and hence W_1 is nothing but square root of C_1 square plus U_1 square and we get 15.61 metres per second. So now we have obtained or it was given to us C_2 U_2 W_2 and U_1 C_1 W_1 , so we can find out the degree of reaction as U_2 square minus U_1 square plus W_1 square minus W_2 square divided by C_2 square minus C_1 square plus U_2 square minus U_1 square plus W_1 square minus W_2 square and that will give me our or the degree of reaction as 0.73.

So these are the some of the problems, while solving these problems on pumps, turbines or any Turbo machine, please keep in mind that you should draw a neat picture of the velocity triangles and try to draw the angles, not, you do not have to make it exact but try to make it looking close. For example if β_2 is given as some value which is acute, try to draw it acute because then you will have a proper idea of how CU 2 is working, is it more or less and then try to work out the triangles properly and get what are the informations which are missing.

And rest of the problem is actually application of suitable formulae. The crux or the most important part of Turbo machine that we will be covering here, we have covered so far and we will be covering in the coming lectures is understanding a problem, translating that problem into suitable velocity triangles and determining different components and then plugging these components into the relationships as we have done here. I hope that if you do the tutorials, these portions will become clearer.

In the next week we will start the pumps and we will revisit some of the problems that we did today in more details. We will talk about the pump performance and the related problems and some of the concepts that we did here will also become more relevant and more meaningful with the practical example of pump. Thank you.