

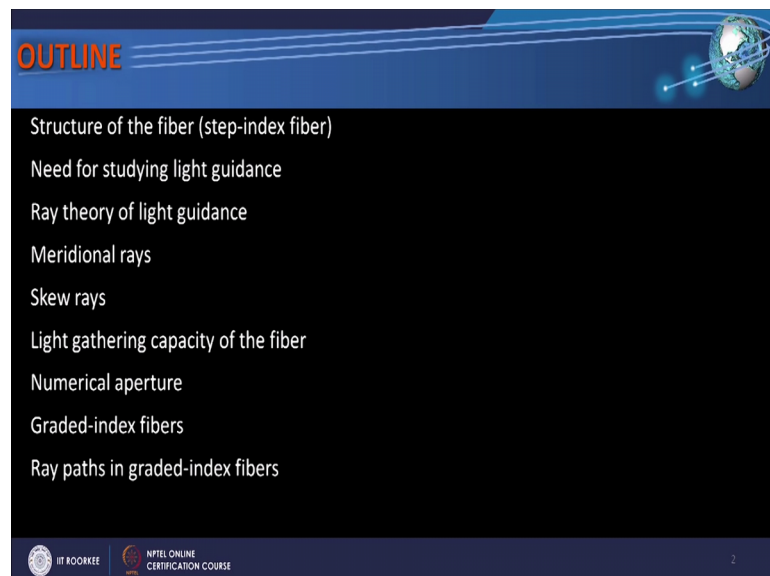
Fiber Optics
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Lecture – 03
Salient Features of Optical Fiber – I

In the last lecture we had answered the question, why do we need optical communication, that is why do we require light waves for telecommunication. And the answer we found is if we utilize carrier wave communication through em waves for telecommunication purpose. And we had seen that in carrier wave communication if we increase the frequency of the carrier, the data transmission rate can be increased the bandwidth of the system increases. Light waves have much larger frequency as compared to the microwaves and radio waves, that is why light waves can give you a enormous bandwidth very large bandwidth, and this is the primary reason for using light waves for high data rate communication. If we want to use light for communication then we need to guide light across curves and corners, in the same way as copper wire conducts electricity.

So, now in this lecture we will look at the structure which carries light along it around all the curves and corners, and this structure is called optical fiber, we are going to look into the salient features and characteristics of optical fiber in this lecture.

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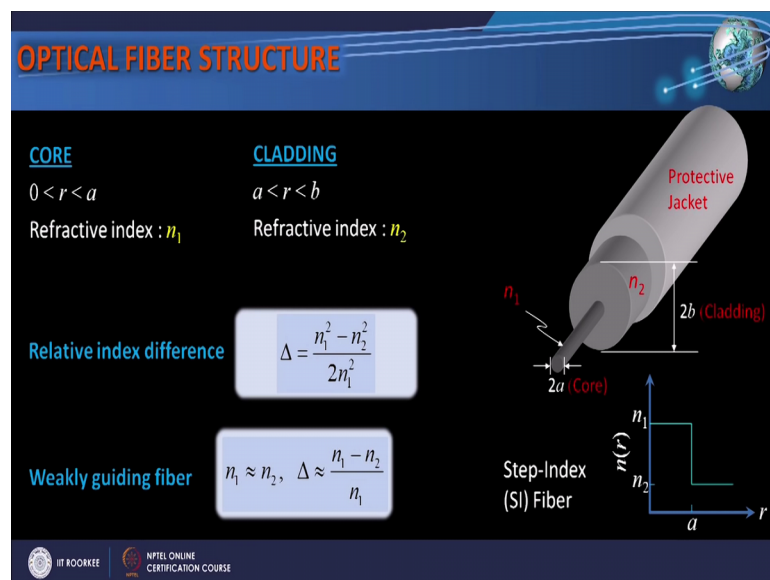
OUTLINE

- Structure of the fiber (step-index fiber)
- Need for studying light guidance
- Ray theory of light guidance
- Meridional rays
- Skew rays
- Light gathering capacity of the fiber
- Numerical aperture
- Graded-index fibers
- Ray paths in graded-index fibers

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So, what plan we have for this lecture, we will look at the structure of a typical optical fiber which is step index fiber then we will understand what is the need for studying light guidance in an optical fiber. What is the ray theory of light guidance which is a very simple theory to understand light guidance in a fiber, fiber guides light through two types of rays one is meridional rays another is skew rays, then what is the light gathering capacity of the fiber, what is the numerical aperture of the fiber, then there are different type of fibers which have refractive index variation in the core they are known as graded index fiber, and we would look into how rays go in graded index fiber, what path they follow.

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So, let us first look at the structure of a typical optical fiber. This fiber has a high index core of refractive index n_1 and radius a , it is surrounded by a cladding of refractive index n_2 and radius b . So, if I look at the refractive index variation in this region, then in the core which is defined by $0 < r < a$, the refractive index is n_1 in the cladding which is defined by $a < r < b$, refractive index is n_2 and this is the refractive index profile of the fiber, $n(r)$ function of r where the refractive index is n_1 from 0 to a , and refractive index is n_2 for r greater than a for simplicity I have considered here infinitely extended cladding instead of a finite cladding because the cladding is much larger cladding dimensions are much larger than the dimensions of the core. So, we can consider it to be infinitely extended.

The index difference between the core and the cladding is defined by a parameter relative index difference, Δ is equal to $\frac{n_1^2 - n_2^2}{2n_1^2}$ and for practical fibers, n_1 is close to n_2 the difference between n_1 and n_2 is small and they are known as weakly guiding fiber for such fibers Δ can be approximated by $\frac{n_1 - n_2}{n_1}$. Now the question is what is the need for studying light guidance in the fiber. Well when we send data through optical fiber it is sent through train of optical pulses, and we need to know what happens to these pulses when they travel through optical fiber.

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NEED FOR STUDYING LIGHT GUIDANCE

Data through optical fiber is sent through train of optical pulses

What happens to light pulses when they travel through optical fiber?

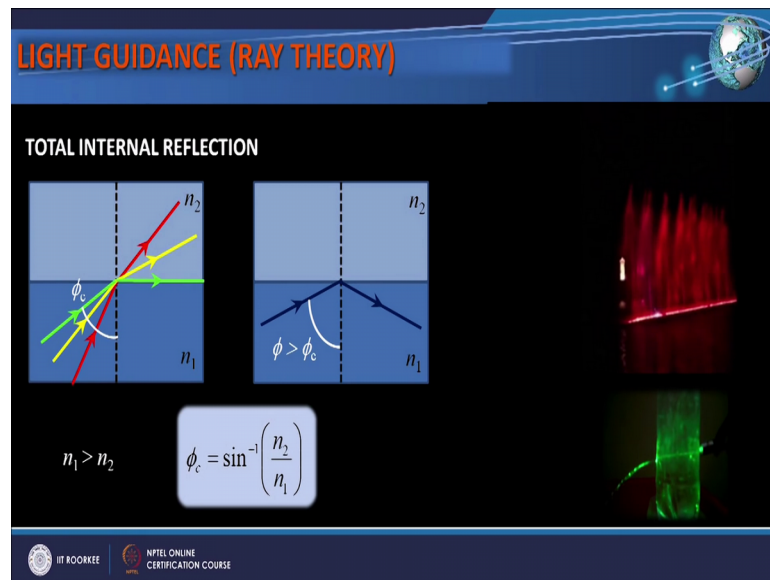
How can we optimize fiber parameters as per our requirements?

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So, studying light guidance through optical fiber and its transmission characteristics, enable us to understand number one what happens to light pulses when they travel through optical fiber, and number two how can we optimize fiber parameters as per our requirements. How light is guided through optical fiber well to understand that.

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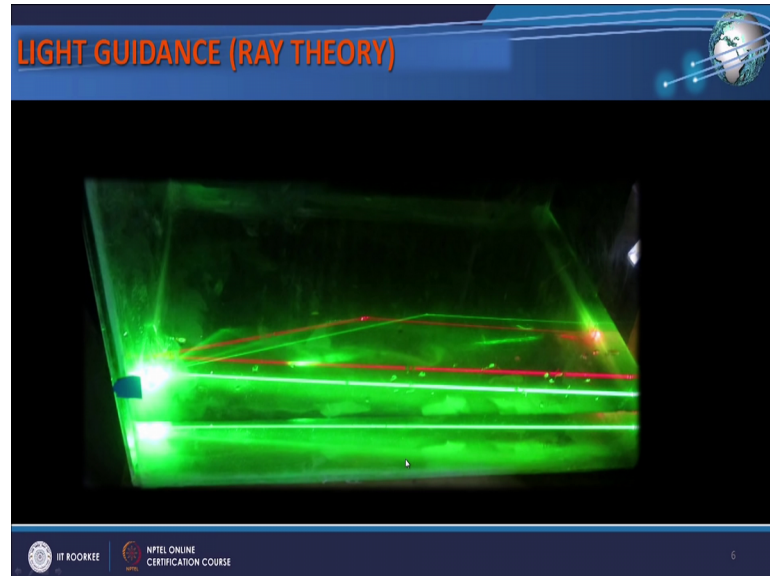


Let us have a look at this which is light at fountain here, and what we see that light is placed somewhere here light source is placed somewhere here and these streams of water they capture light they are lighted all over. How do they capture light how do they guide light along the stream how the light is guided along the stream. Another thing we can look at is we can perform a very simple experiment in which we fill a transparent bottle with water, pierce a small hole in the bottle and let the water stream come out. Now if I launch light from a laser pointer on to this hole, then what I see that here the light travels in a straight line, but here this is stream of water captures light, and light is guided along the stream how this light is guided at all well. The answer is the mechanism of guidance here is total internal reflection what is total internal reflection. So, to understand that let us have let us have these two media n₁ and n₂, this is a denser medium this is a rarer medium. So, n₁ is greater than n₂.

Now, when a light ray is incident on the interface of these two media, the light ray gets reflected. If I increase the angle of incidence from the normal, then since it is going from denser to rarer it moves away from the normal. So, if I increase the angle it will further move away from the normal and at one particular angle φ_c this reflected ray basically grazes the interface between the two media. Now what is this φ_c. This φ_c is called the critical angle for total internal reflection and it can be given by sin inverse n₂ over n₁. Now if I incident a light ray which makes an angle larger than φ_c then this light comes back into the same medium this is known as total internal reflection and the

condition for total internal reflection is that ϕ should be greater than ϕ_c the critical angle.

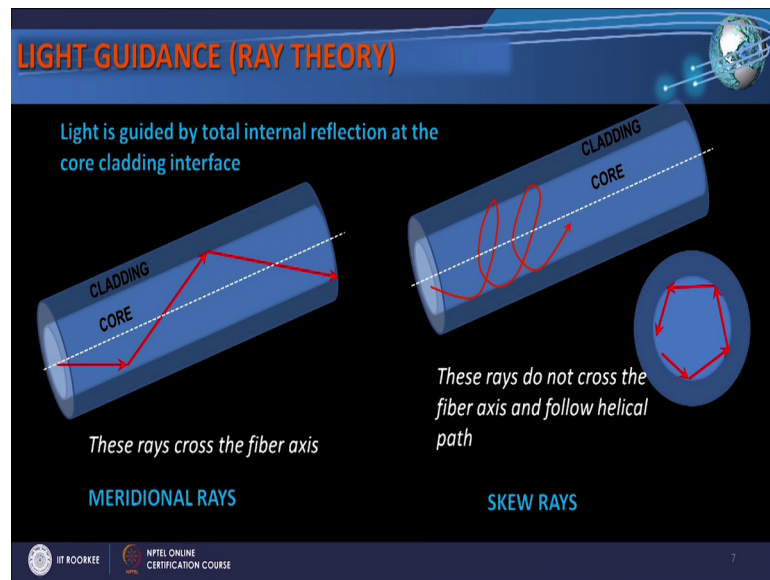
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This is one very simple experiment that you can do you can fill a transparent tank with water and then you send the laser beam at different angles, and you find that if the angle of incidence is larger than the critical angle there is total internal reflection at the interface of water and air.

Now, if I look at the ray theory of light guidance in optical fiber, then light is guided by total internal reflection at core cladding interface.

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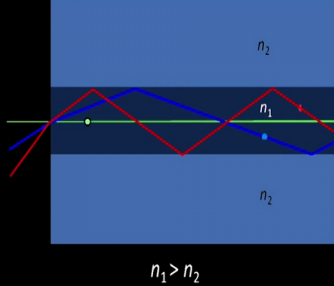
So, if I launch a ray of light into the fiber it goes like this, and if this angle this angle which it this ray makes with the normal to the core cladding interface is larger than the critical angle, then it will be total internally reflected and it would be guided. What we can see here is these rays they cross the fiber axis and these are known as meridional rays there can be another possibility that depending upon the launch conditions, a ray can never cross the fiber axes, but it will be totally internally reflected it will undergo TIR, but it will follow on a helical path it will never cross the fiber axis. If these would be clear when we see the transfers cross section of the fiber, if I look at transfers cross section. So, these rays go like this and they never cross the axes. So, these rays are known as a skew rays. So, light guidance takes place via meridional rays as well as a skew rays in an optical fiber.

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RAY THEORY (MERIDIONAL RAYS)

Ray Theory : Total Internal Reflection (meridional rays)

Longitudinal cross section of the fiber



Light launched at various angles from the fiber axis is guided through successive total internal reflection.

Are the rays launched at all the angles guided?

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Now, let us look at light guidance by meridional rays. So, if I launch light at various angles into this fiber this is a longitudinal cross section of the fiber, then what happens is that the rays launched at different angles will be guided through successive total internal reflections. Now the question is are the rays launched at all the angles guided or there are only certain range of angles that would be guided.

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RAY THEORY (MERIDIONAL RAYS)

CONDITION FOR TIR

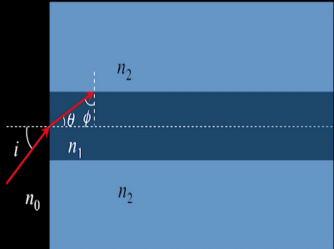
Let a ray of light be incident from medium of refractive index n_0 on the input end at axial point (centre) of the fiber

$$n_0 \sin i = n_1 \sin \theta$$

Critical angle at core-cladding interface is given by

$$\sin \phi_c = \frac{n_2}{n_1}$$

For TIR at core-clad interface $\phi > \phi_c$ OR $\frac{\pi}{2} - \theta > \phi_c$



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To understand that let us apply the condition for total internal reflection in the fiber. So, again this is the longitudinal cross section of the fiber, you have a core with refractive

index n_1 and cladding of refractive index n_2 this is the fiber axis, and the refractive index of the outside medium is n_0 .

Now, let me launch a ray from outside medium onto the input end of the fiber, let us say at an axial point and it makes an angle i from the axis of the fiber. Now when this ray enters the fiber it is refracted, and like this reflected ray make an angle θ from the fiber axis and correspondingly an angle ϕ with the normal to the interface of core and cladding. Now from Snell's law I know that $n_0 \sin i$ should be equal to $n_1 \sin \theta$, and the critical angle at core cladding interface is given by $\sin \phi_c$ is equal to n_2 over n_1 . Now it is clear that for TIR at core cladding interface this ϕ should be greater than ϕ_c and correspondingly $\pi/2 - \theta$ should be greater than ϕ_c because this ϕ is equal to $\pi/2 - \theta$. So, if this ϕ is greater than ϕ_c or this $\pi/2 - \theta$ is greater than ϕ_c , then this ray will undergo TIR successive TIR at core cladding interface and would be guided.

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RAY THEORY (MERIDIONAL RAYS)

CONDITION FOR TIR & LIGHT ACCEPTANCE ANGLE

For TIR at core-clad interface

$$\frac{\pi}{2} - \theta > \phi_c \quad \text{or} \quad \theta < \frac{\pi}{2} - \phi_c$$

→ $\sin \theta < \cos \phi_c$ or $n_1 \sin \theta < n_1 \cos \phi_c$

→ $n_0 \sin i < n_1 \sqrt{1 - \frac{n_2^2}{n_1^2}}$ or $\sin i < \frac{\sqrt{n_1^2 - n_2^2}}{n_0}$

$\sin i_{\max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0}$ defines the maximum acceptance angle

for outside medium air $n_0 = 1$

$$\sin i_{\max} = \sqrt{n_1^2 - n_2^2}$$

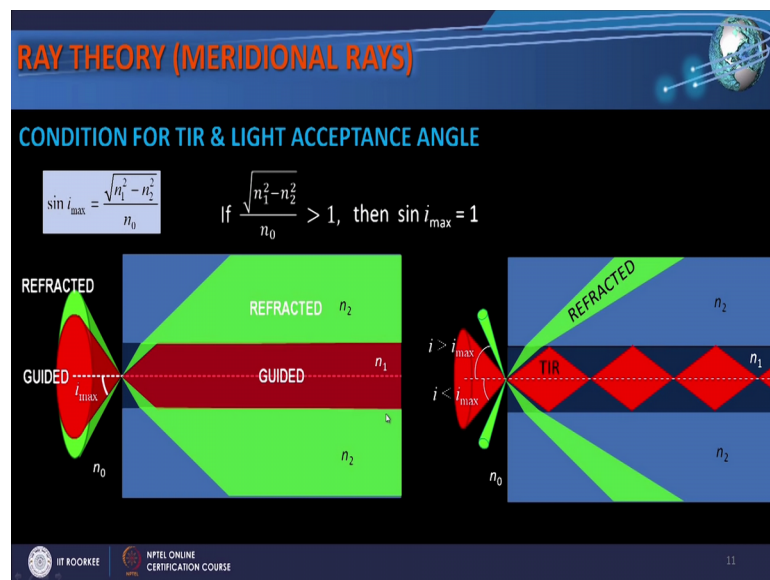
The diagram shows a cross-section of a fiber with core refractive index n_1 and cladding refractive index n_2 . A ray enters from an outside medium with refractive index n_0 at an angle i to the axis. Inside the core, it refracts to an angle θ to the axis and an angle ϕ to the normal at the core-cladding interface. The critical angle ϕ_c is also indicated.

This condition for total internal reflection can also be written as θ is less than $\pi/2 - \phi_c$, and now if I take sin of this then $\sin \theta$ should be less than $\cos \phi_c$ and if I multiply it by n_1 then $n_1 \sin \theta$ should be less than $n_1 \cos \phi_c$, since $\sin \phi_c$ is equal to n_2 over n_1 . So, $\cos \phi_c$ would be equal to square root of $1 - n_2^2$ over n_1^2 . So, $n_1 \sin \theta$ is equal to $n_0 \sin i$. So, this equation will now give me $n_0 \sin i$ should be less than $n_1 \sqrt{1 - n_2^2 / n_1^2}$ or $\sin i$

should be less than square root of $n_1^2 - n_2^2$ over n_0 . So, for a limiting case if I consider the limiting case, this $\sin i_{\max}$ is equal to square root of $n_1^2 - n_2^2$ over n_0 defines the maximum acceptance angle; which means that if this i is less than i_{\max} then there would be total internal reflection at core cladding interface and light could be guided through optical fiber.

If I take outside medium as air then n_0 is equal to 1, and $\sin i_{\max}$ is equal to square root of $n_1^2 - n_2^2$. Now we have seen that $\sin i_{\max}$ is given by this the question is if $n_1^2 - n_2^2$ over n_0^2 is greater than 1 then what would be i_{\max} or $\sin i_{\max}$.

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As I know that $\sin i_{\max}$, i_{\max} cannot assume values greater than 1. So, even if it is greater than one then $\sin i_{\max}$ will be kept at value one because i_{\max} cannot be greater than ninety degrees. So, now, if I launch a cone of light into the fiber, then what I see that all the light which lies in the cone of semi vertical angle i_{\max} will be guided through the core of the fiber and the light which makes angles larger than i_{\max} would be refracted. I can see it in this way also that if this cone of light has semi vertical angle which makes with which is smaller than i_{\max} , then this light will be guided through total internal reflection and if I launch light in this region where the angles are larger than i_{\max} then this light will be refracted, and it will not be guided through optical fiber.

The second kind of rays which we talked about is skew rays. What is the condition for total internal reflection and light acceptance angle what for skew rays for that let me launch a ray of light somewhere here on to the fiber end and it makes an angle I with the fiber axis in the outside medium n_0 when it enters the fiber this ray makes an angle theta with the longitudinal direction of the fiber, and it is reflected here.

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RAY THEORY (SKEW RAYS)

CONDITION FOR TIR & LIGHT ACCEPTANCE ANGLE

Since, $PQ \cos \phi = SQ$, $QT \cos \alpha = SQ$ and $PQ \sin \theta = QT$

$$SQ = PQ \sin \theta \cos \alpha$$

and thus

$$\cos \phi = \sin \theta \cos \alpha$$

For limiting case of TIR

$$\phi = \phi_c, \theta = \theta_c \text{ and } i = i_{\max}$$

and so

$$\cos \phi_c = \sin \theta_c \cos \alpha \quad \text{since } \sin \phi_c = n_2/n_1, \text{ it gives } \sin \theta_c \cos \alpha = \sqrt{1 - \frac{n_2^2}{n_1^2}}$$

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It is incident it hits the point Q at core cladding interface and then it is reflected. Let me make this plane consider this plane which contains this incident light and reflected light which is represented by green here, and this is the normal QT is the normal at the core cladding interface and then let me also consider another plane which is a longitudinal plane, but which contains this line this longitudinal line which passes through Q.

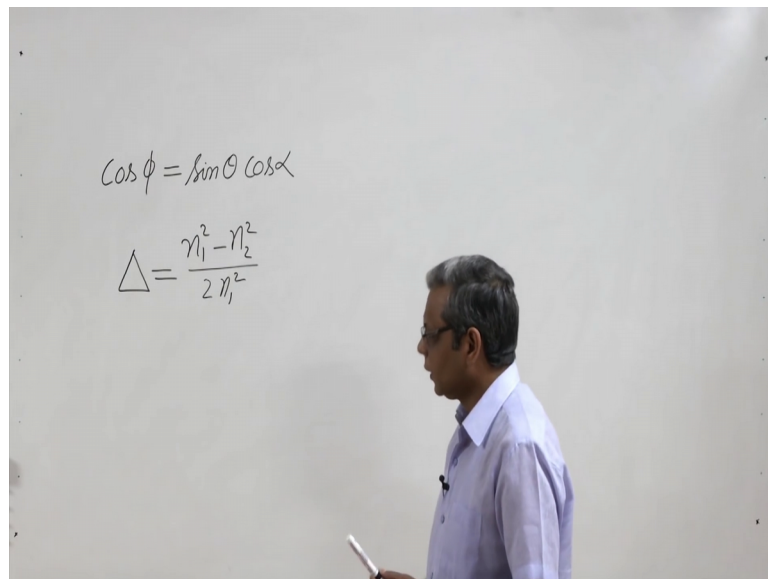
So, basically this plane makes an angle alpha from this longitudinal plane, if I consider a transverse plane here which is SPQ, then this transverse plane makes an angle phi from this incident ray and this is the reflected ray that also makes an angle phi with this. Now what I can see here is that this $PQ \cos \phi$ is nothing, but SQ and $QT \cos \alpha$ is also SQ I also find that this $PQ \sin \theta$ is QT . So, if I considered these two then I find that this SQ is nothing, but $PQ \sin \theta \cos \alpha$, because $QT \cos \alpha$ is equal to SQ and QT is $PQ \sin \theta$ here.

Now, if I consider these two equations I compare them then I immediately get $\cos \phi$ is equal to $\sin \theta \cos \alpha$. So, in this way what I have got I have got ϕ , in terms of

theta and alpha theta is related to i. So, I can relate it to I and then I can find out what is the condition of total internal reflection I know that for total internal reflection phi should be greater than phi c, and if I consider this limiting case for TIR then phi is equal to phi c correspondingly theta is equal to theta c, and let us say i is equal to imax. Then I have from here cos phi c is equal to sin theta c cos alpha, and since phi c is equal to n 2 over n 1 it gives me sin theta c cos alpha is equal to square root of n 2 square over n 1 square from here.

So, let me write this one down which I will use later also that cos phi cos phi is equal to sin theta cos alpha. So, cos phi is equal to sin theta cos alpha.

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Now, since from Snell's law, I have already seen that n 0 sin I should be equal to n 1 sin theta. So, n 0 sin imax should be equal to n 1 sin theta c correspondingly.

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RAY THEORY (SKEW RAYS)

CONDITION FOR TIR & LIGHT ACCEPTANCE ANGLE

Since $n_0 \sin i = n_1 \sin \theta$, $n_0 \sin i_{max} = n_1 \sin \theta_c$

Hence $\sin i_{max} = \frac{n_1 \cos \phi_c}{n_0 \cos \alpha} = \frac{n_1}{n_0 \cos \alpha} \sqrt{1 - \frac{n_2^2}{n_1^2}} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0 \cos \alpha}$

Recall that in the case of meridional rays $\sin i_{max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0}$

→ skew rays are accepted for TIR at larger axial angles than the meridional rays

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And hence $\sin i_{max}$ would be equal to $n_1 \cos \phi_c$ over $n_0 \cos \alpha$, because $\sin \theta$ is equal to $\cos \phi_c$ divided by $\cos \alpha$. So, and $\cos \phi_c$ is square root of $1 - n_2^2$ over n_1^2 . So, this gives me $\sin i_{max}$ is equal to square root of $n_1^2 - n_2^2$ over $n_0 \cos \alpha$. You just recall that in case of meridional rays this $\sin i_{max}$ was a square root of $n_1^2 - n_2^2$ over n_0 . Now I have an extra factor of $\cos \alpha$ in denominator, and $\cos \alpha$ has maximum value one and that is the limiting case. So, since $\cos \alpha$ is less than one for skew rays. So, skew rays are accepted for TIR at larger angle than the meridional rays.

What happens is that these skew rays are confined to the rim of the fiber, they never cross the axis and therefore, they do not fully utilize core for light guidance and because of this they are not very important to be considered in optical fiber design and communication.

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RAY THEORY

NUMERICAL APERTURE

We have seen that the rays launched into the fiber are limited to a maximum acceptance angle for guidance through the fiber.

$$\sin i_{max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0} \quad (\text{Meridional rays}) \quad \sin i_{max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0 \cos \alpha} \quad (\text{Skew rays})$$

For $n_0 = 1$ (air) for meridional rays $\sin i_{max} = \sqrt{n_1^2 - n_2^2}$ represents max. acceptance angle or light gathering capacity of the fiber and is referred to as numerical aperture (NA)

$$NA = \sqrt{n_1^2 - n_2^2} \quad \text{or} \quad NA = n_1 \sqrt{2\Delta}$$

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Now, let us look at numerical aperture of the fiber, we have seen that the rays launched into the fiber are limited to a maximum acceptance angle for guidance through optical fiber. For meridional rays this acceptance angle is given by $\sin i_{max} = \frac{\sqrt{n_1^2 - n_2^2}}{n_0}$ and for skew rays it is $\frac{\sqrt{n_1^2 - n_2^2}}{n_0 \cos \alpha}$.

Now, if outside medium is air then for meridional rays $\sin i_{max}$ is equal to $\sqrt{n_1^2 - n_2^2}$, and this represents the numerical aperture of the fiber. So, if the fiber is in air, then what is the maximum acceptance angle that gives you the numerical aperture of the fiber. Because this maximum at maximum acceptance angle basically tells you the light gathering capacity of the fiber and that is why it gives you the numerical aperture it is known as numerical aperture of the fiber. So, numerical aperture or in short NA is a square root of $n_1^2 - n_2^2$ and it purely depends upon the refractive indices of the core and the cladding.

If you remember that I had defined relative core cladding index difference Δ is equal to $\frac{n_1^2 - n_2^2}{2n_1^2}$. So, I can represent this NA also in terms of Δ . So, you get it as $NA = n_1 \sqrt{2\Delta}$. Let us consider an example for a typical glass fiber with $n_1 = 1.45$ and $n_2 = 1.44$ Δ is equal to about 0.69 percent and NA is equal to 0.17.

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RAY THEORY

EXAMPLE

For a typical glass fiber with $n_1 = 1.45$ and $n_2 = 1.44$

$$\Delta = \frac{n_1^2 - n_2^2}{2n_1^2} = 0.0069 \text{ or } 0.69\% \quad NA = \sqrt{n_1^2 - n_2^2} = 0.17$$

Max. acceptance angle in air ($n_0 = 1$)

Max. acceptance angle in water ($n_0 = 1.33$)

Meridional rays: $i_{max} = \sin^{-1} \frac{NA}{n_0} = 9.8^\circ$

Meridional rays: $i_{max} = 7.3^\circ$

Skew rays ($\alpha = 40^\circ$)

Skew rays ($\alpha = 40^\circ$)

$$i_{max} = \sin^{-1} \left(\frac{NA}{n_0 \cos \alpha} \right) = 12.8^\circ$$
$$i_{max} = 9.6^\circ$$

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The maximum acceptance angle in air is can now be given by for meridional rays as i_{max} is equal to $\sin^{-1} \frac{NA}{n_0}$, which is about 10 degrees 9.8 degrees and for skew rays for α is equal to 40 degrees it is about 12.8 degrees. If I put the same fiber in water where the refractive index is 1.33, then for meridian rays i_{max} becomes 7.3 and for skew rays it is 9.6.

So, what do I see here that for any given outside medium the a skew rays have larger i_{max} than meridional rays, and if I change the outside medium if I increase the refractive index of the outside medium, the light acceptance angle goes down.

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RAY THEORY

EXAMPLE

For unclad (air clad) glass fiber : $n_1 = 1.45$ and $n_2 = 1$

$$\Delta = \frac{n_1^2 - n_2^2}{2n_1^2} = 0.2622 \quad \sqrt{n_1^2 - n_2^2} = 1.05 \quad NA = 1$$

This shows that max. acceptance angle for guidance can be close to 90°

Clearly, this fiber would have much larger light gathering capacity than the cladded fiber

Question: *What is the need for cladding?*

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If I consider an unclad fiber than n_1 is equal to 1.45 and n_2 is one which is basically air then Δ is 0.26 and square root of $n_1^2 - n_2^2$ is equal to 1.05 which means NA should be equal to 1. This shows that the maximum acceptance angle for guidance can be close to 90 degrees because NA is equal to 1 $\sin i_{max}$ is equal to 1 clearly this fiber would have much more light gathering capacity as compared to cladded fiber.

Then the question is what is the need for cladding and we will answer this question later in subsequent lectures. Now let us look at the limitations of ray theory what are the limitations of ray theory. Well ray theory is basically geometrical optics and geometrical optics is valid only for dimensions which are much larger than the wavelength of light. So, ray theory basic term.

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RAY THEORY

LIMITATIONS OF RAY THEORY

- ✓ Geometrical optics is valid only for dimensions much larger than the wavelength of light. The ray theory, therefore, breaks down for core size comparable to wavelength of light.
- ✓ It does not tell about the discrete modes of the fiber.
- ✓ When light is guided through the fiber, some light also extends to the cladding. The ray theory cannot explain this.

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When we consider fiber whose core is of the order or to the comparable to the wavelength of light. Second thing that it will not tell you the discrete modes of the fiber as we will go along we will learn that the fiber support certain discrete modes of propagation, but ray theory cannot tell you about discrete modes of the fiber. Third thing is when light is guided through optical fiber, some light also extends to the cladding and ray theory cannot explain this. So, these are some limitations of the ray theory.

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GRADED-INDEX (GI) FIBER

The refractive index of the core is not uniform. It varies with r

A convenient way of defining the radially varying refractive index is by using *power-law profile*

$$n(r) = \begin{cases} n_1 \left[1 - 2\Delta \left(\frac{r}{a} \right)^q \right]^{1/2} & ; r < a \\ n_2 & ; r > a \end{cases}$$

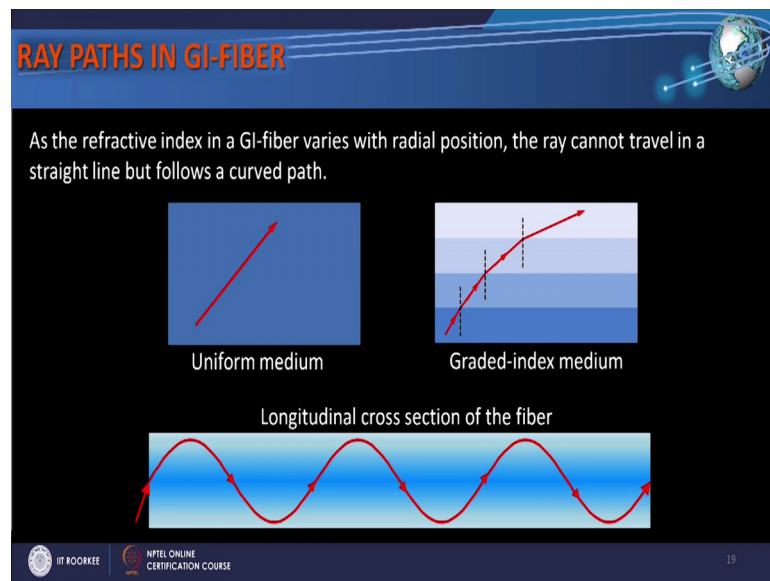
q is the profile parameter

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Then apart from step index fibers there are graded index fibers where the refractive index of the core is not uniform, it varies with r the radial position. And a convenient way of defining this radially varying refractive index is using power law profile which is given as $n(r)$ is equal to $n_1 \sqrt{1 - 2\Delta (r/a)^q}$ for r less than a and it is equal to n_2 for r greater than a in the cladding. This q is nothing, but profile parameter, it basically governs the index gradation let us see what does it mean.

So, if I put q is equal to 1, then the refractive index profile would be something like this in the core as you move away from the axis, the refractive index will gradually decrease and this decrease is linear this is also known as triangular profile. If q is equal to 2 then this decrease is like this in parabolic fashion, then this fiber is also known as parabolic index profile fiber, and if q is very large if q is infinity then this is nothing, but a step index fiber. So, very large values of q will give you a step index profile.

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How the ray paths look like in a graded index fiber. If I have a uniform medium and I launch a ray of light from here it goes straight, but in a graded index medium there is change in refractive index here the refractive index is larger than a smaller than a smaller than smaller, then what happens is if you consider an interface here like this then it will move away from the normal, then here again away from the normal here again away from the normal. So, light will not go straight, but it will be banned. So, it will follow a

curved path and this is the ray path in a typical parabolic index fiber if the refractive index is parabolic away from the axis, then the ray launched into the fiber follows a sinusoidal kind of path. So, the ray paths are curved.

So, in this lecture what we have understood is how light is guided through optical fiber via meridional rays, and skew rays what is the condition for light guidance, what is the light gathering capacity of the optical fiber, what is the numerical aperture of the fiber, what happens to the numerical aperture when the outside medium refractive index changes and what are graded index fibers.

Thank you.